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BRASÍLIA (DF) - BRASIL

# Impact of Induction Motor Loads into Voltage Stability Margins of Large Systems – Rio Area Analysis

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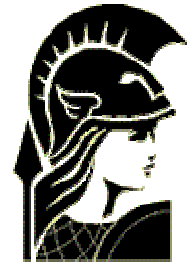
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# Presentation Summary

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- ▶ Introduction
- ▶ Motor Modeling in Power Flow Studies
- ▶ Illustrative Example
- ▶ Maximum Loadability Assessment – Rio Area
- ▶ Conclusions



## Introduction

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- ▶ Blackouts are result of voltage instability/collapse
- ▶ These events may occur due to exhaustion of the system reactive power reserves
- ▶ The analysis requires adequate methodologies and efficient software
  - ▶ Continuation Power Flow, analysis of P-V and Q-V curves



## Motivation

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- ▶ Rio Area during hot summer days of '97
  - ▶ Air-conditioning systems highly used
  - ▶ Depressed voltage conditions despite active loading below the expected critical values
- ▶ Preliminary conclusions
  - ▶ Representing loads by constant-P and constant-I models was not adequate
  - ▶ Inductions motors should be better modeled



# Motor Modeling in Power Flow Studies

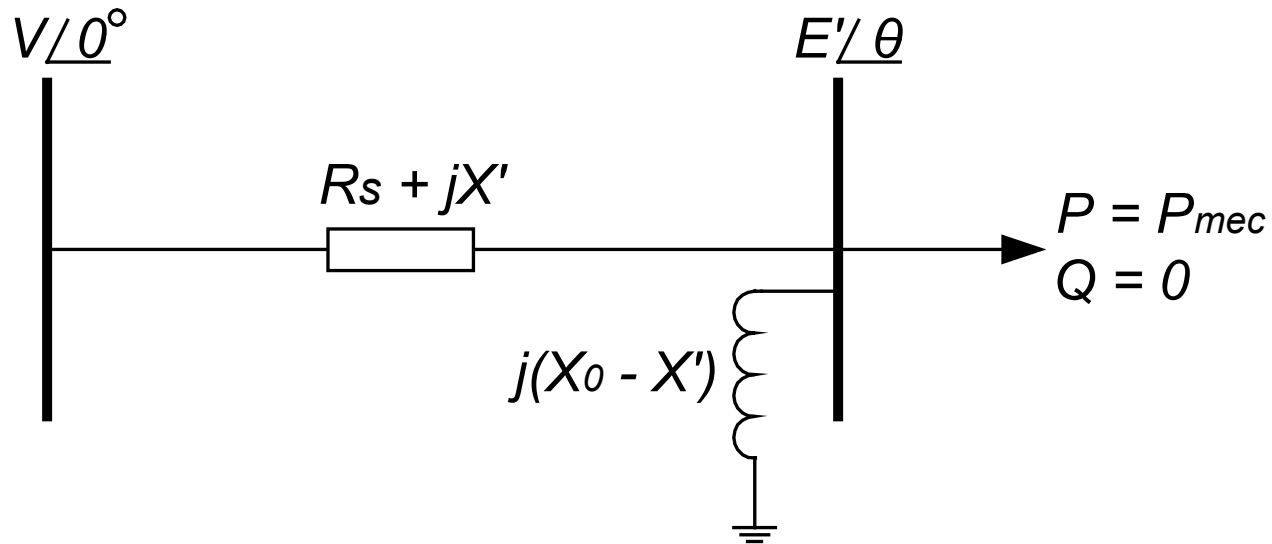
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- ▶ Implementation of aggregate induction motor models into a continuation power flow program
- ▶ Motor models – several types and typical parameters embedded in the program code
- ▶ User must specify the motor type and the content in each load bus
- ▶ Testing
  - ▶ Loadability studies of the Rio Area



# Motor Modeling in Power Flow Studies

- ▶ Two-bus steady-state model for induction motors



- ▶ The mechanical torque is assumed independent of rotor speed
- ▶ For each motor, the electrical network is augmented by one bus with an additional shunt element and connected to the terminal bus by an additional impedance



# Motor Modeling in Power Flow Studies

- ▶ Bus Data indicate which motor type will be used and the percentage of load to be modeled as motors

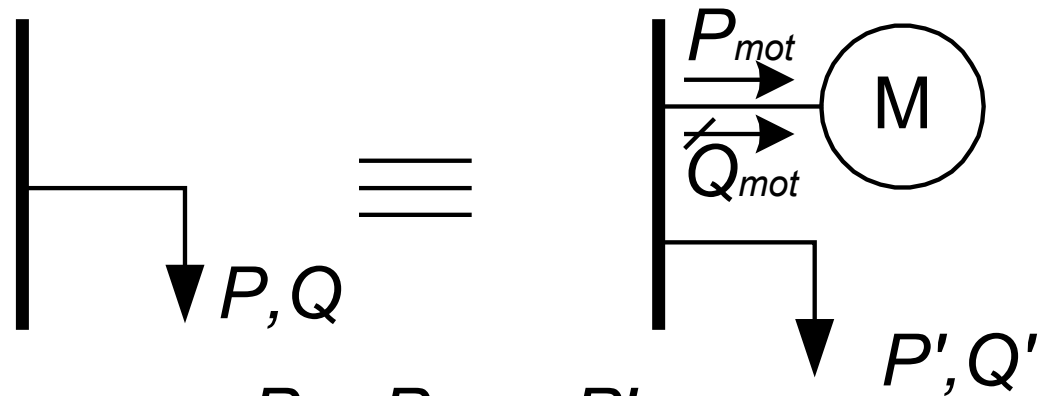
<i>Motor Type</i>	<i>Motor Characteristics</i>
1	Small Industrial I
2	Large Industrial
3	Mean values for 11 kVA motors
4	Small Industrial II
5	Commercial+Feeder
6	Aggregate residential
7	Single Phase



# Motor Modeling in Power Flow Studies

- ▶ MVA Base for each motor is a function of percentage of the load modeled as motor in that particular bus
- ▶ The power flow program calculates
  - ▶ Active and reactive power consumption
  - ▶ Internal voltage  $E'$ , angle  $\theta$ , and rotor slip  $s$

- ▶ The original load which is not modeled as motor is denoted as  $P'$  and  $Q'$



$$P = P_{mot} + P'$$
$$Q = Q_{mot} + Q'$$





# Motor Modeling in Power Flow Studies

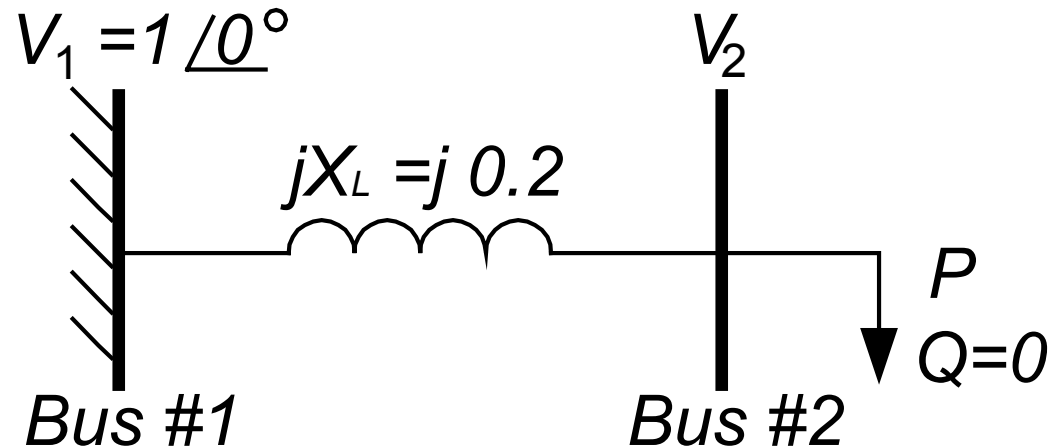
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- ▶ Methodology for continuation power flow studies
  - ▶ Motor load is increased by increasing the MVA motor base
  - ▶ This procedure is equivalent to increasing the number of motors in the system



## Illustrative Example

### ▶ Test System



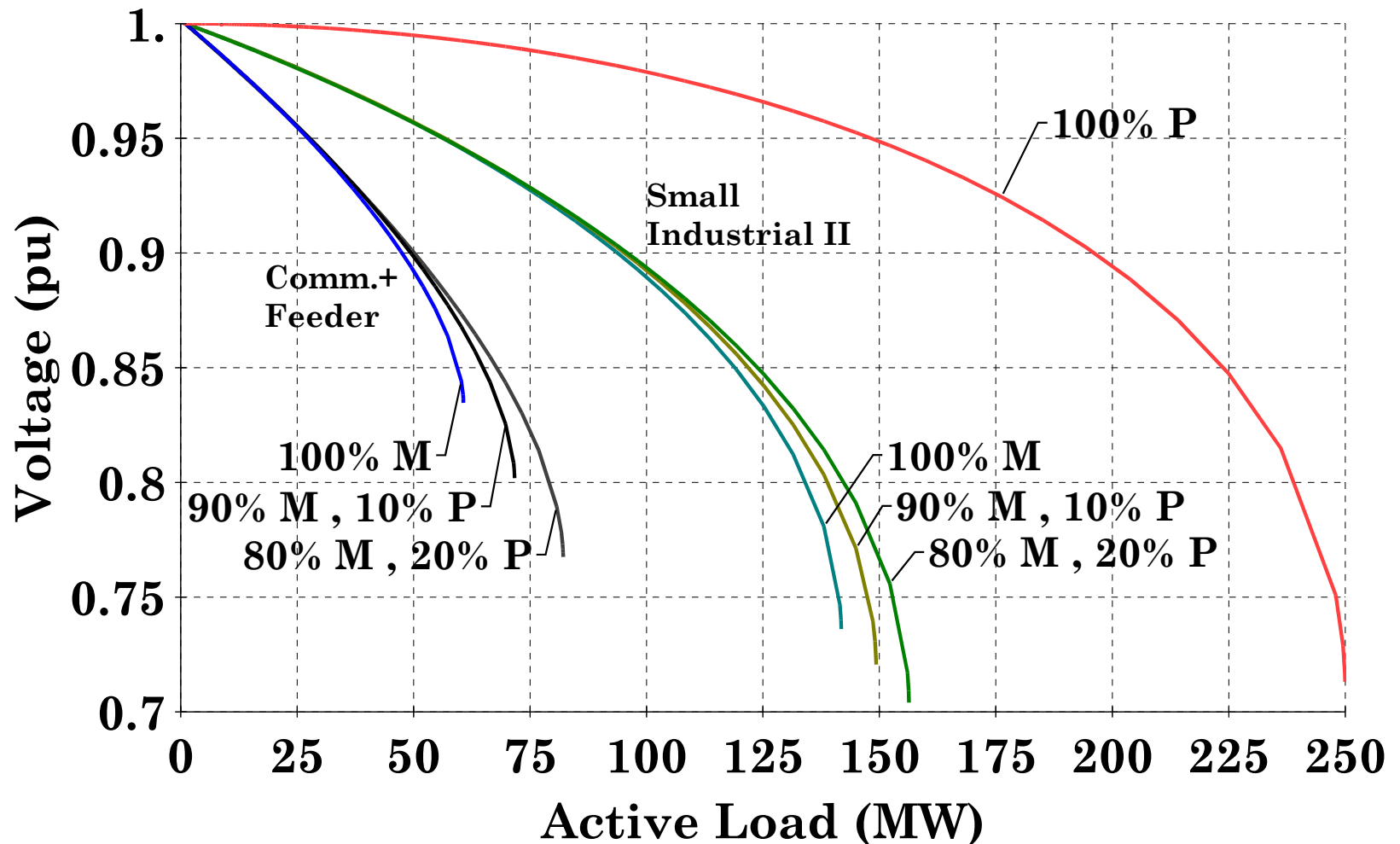
### ▶ Continuation Power Flow

- ▶ Used to obtain maximum loadability for different models of the load at bus #2



## Illustrative Example

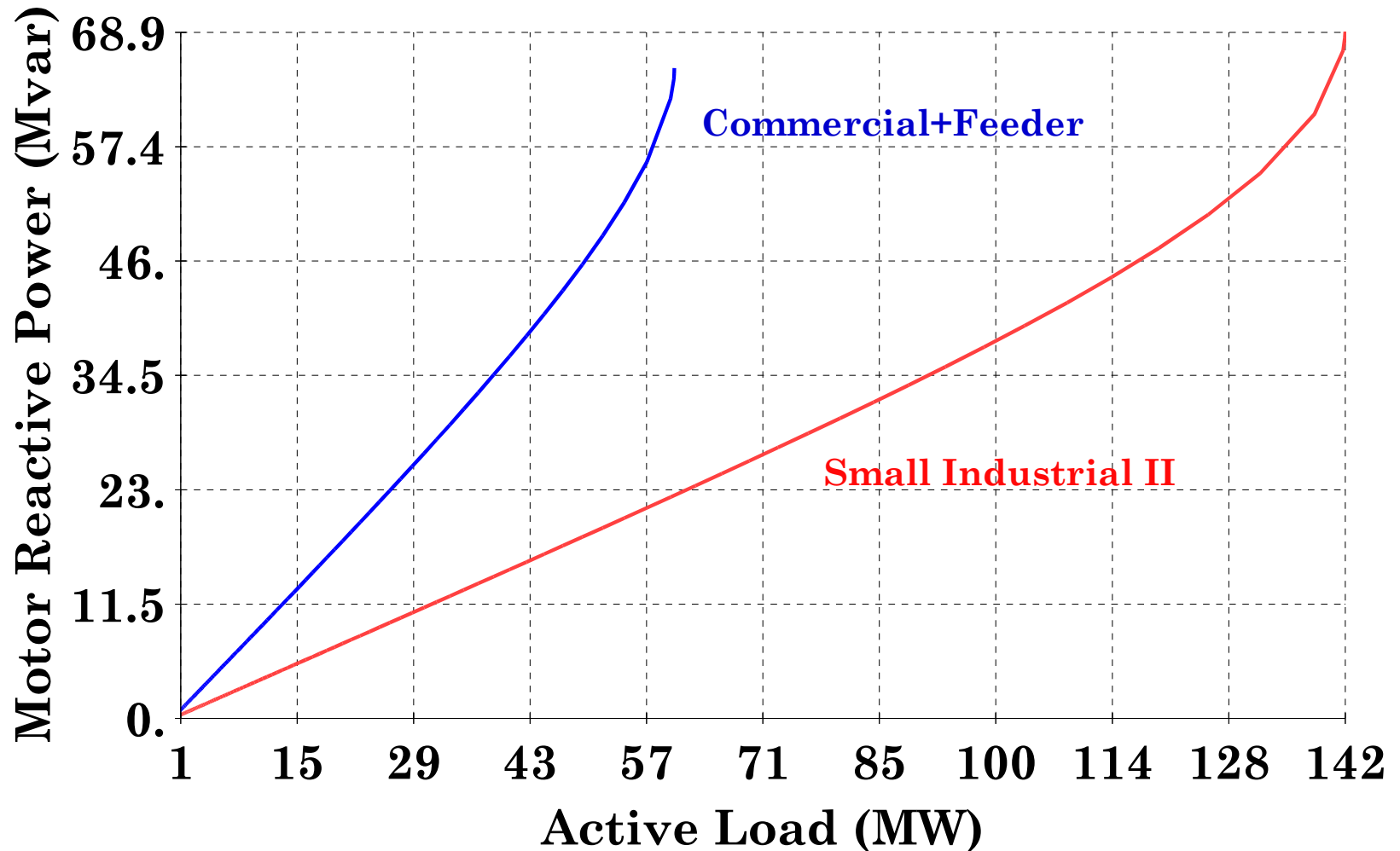
- ▶ PxV Curves for different load models at bus #2





## Illustrative Example

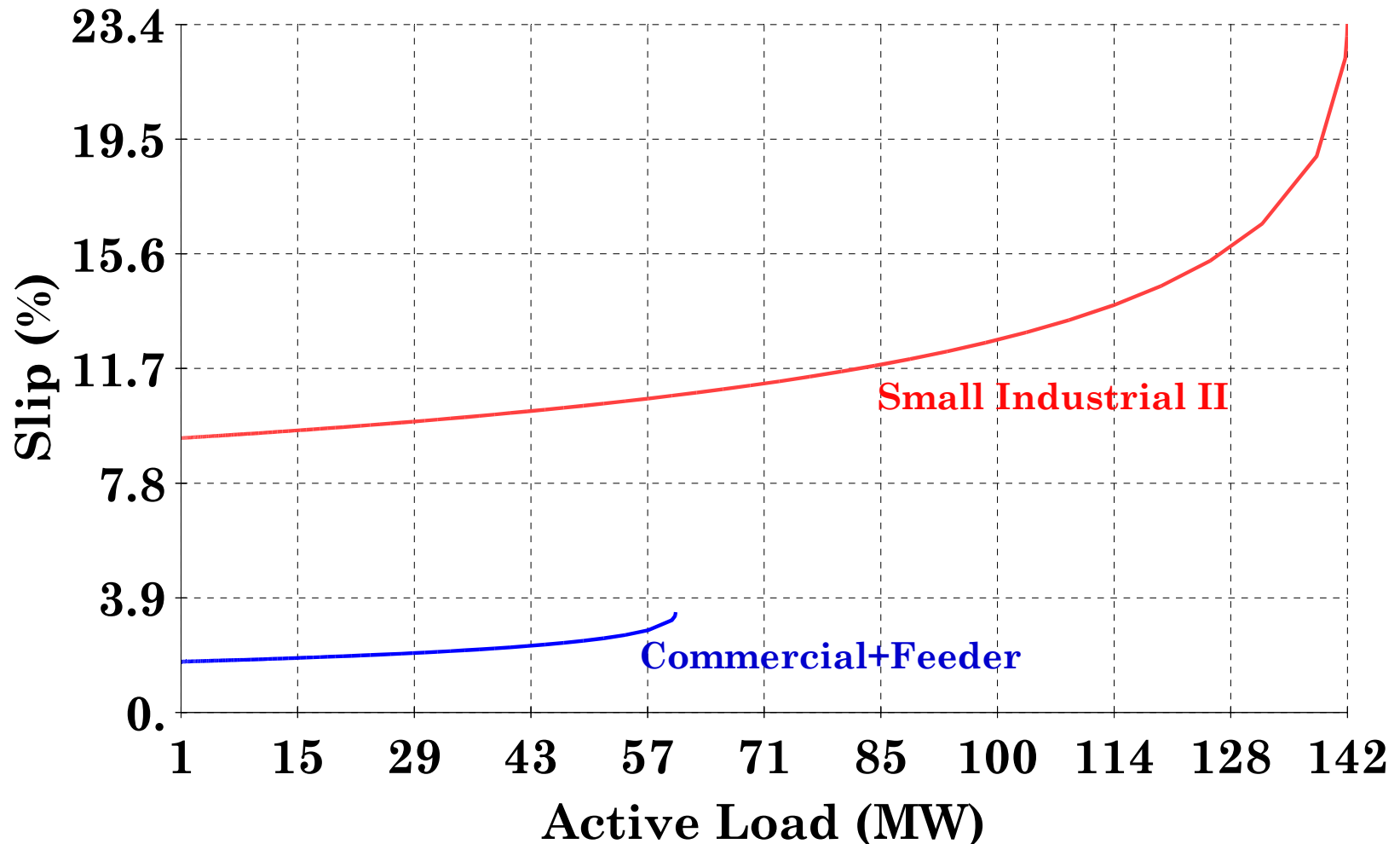
### ► Reactive Power Consumption at bus #2





## Illustrative Example

- ▶ Rotor Slip Curves: two set of induction motor parameters





# Maximum Loadability Assessment - Rio Area

- ▶ Rio Area – 3 utilities: LIGHT, CERJ and ESCELSA
  - ▶ 288 buses
  - ▶ 200 load buses (7632 MW)
  - ▶ 149 buses with load modeled as induction motor (5733 MW)
    - ▶ Industrial: 2227 MW – Comercial: 3506 MW
  - ▶ Operation point refers to a heavy load condition for the Rio Area on a summer day



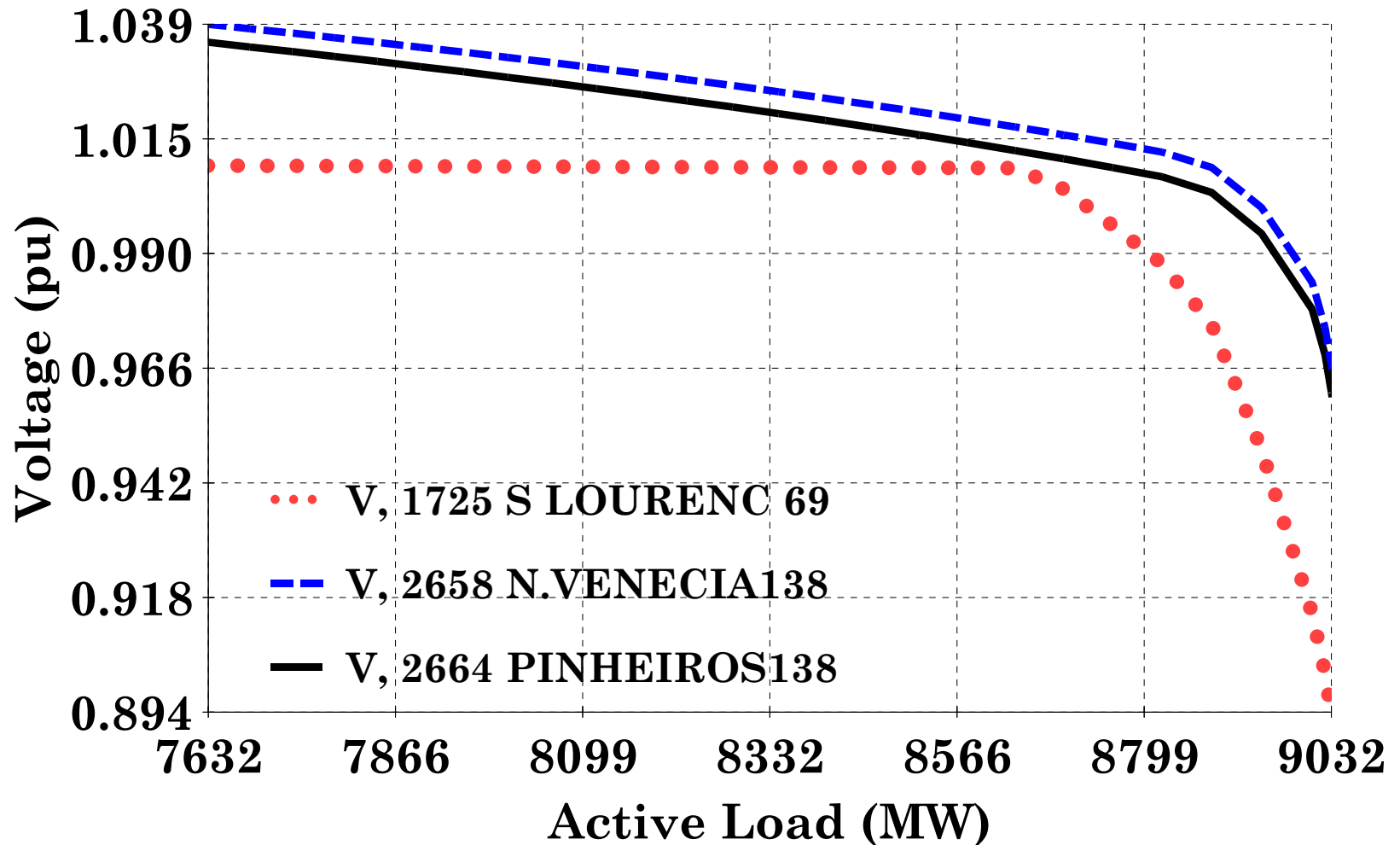
# Maximum Loadability Assessment - Rio Area

- ▶ Other assumptions made in continuation power flow analysis:
  - ▶ Industrial motor load remains constant
  - ▶ Only commercial motor load is increased
  - ▶ Commercial and industrial load is initially modeled as constant P and Q, with fixed power factor
  - ▶ The PxV curves
    - ▶ Most critical buses belong to ESCELSA (distribution utility)



# Maximum Loadability Assessment - Rio Area

► Constant P and Q load model







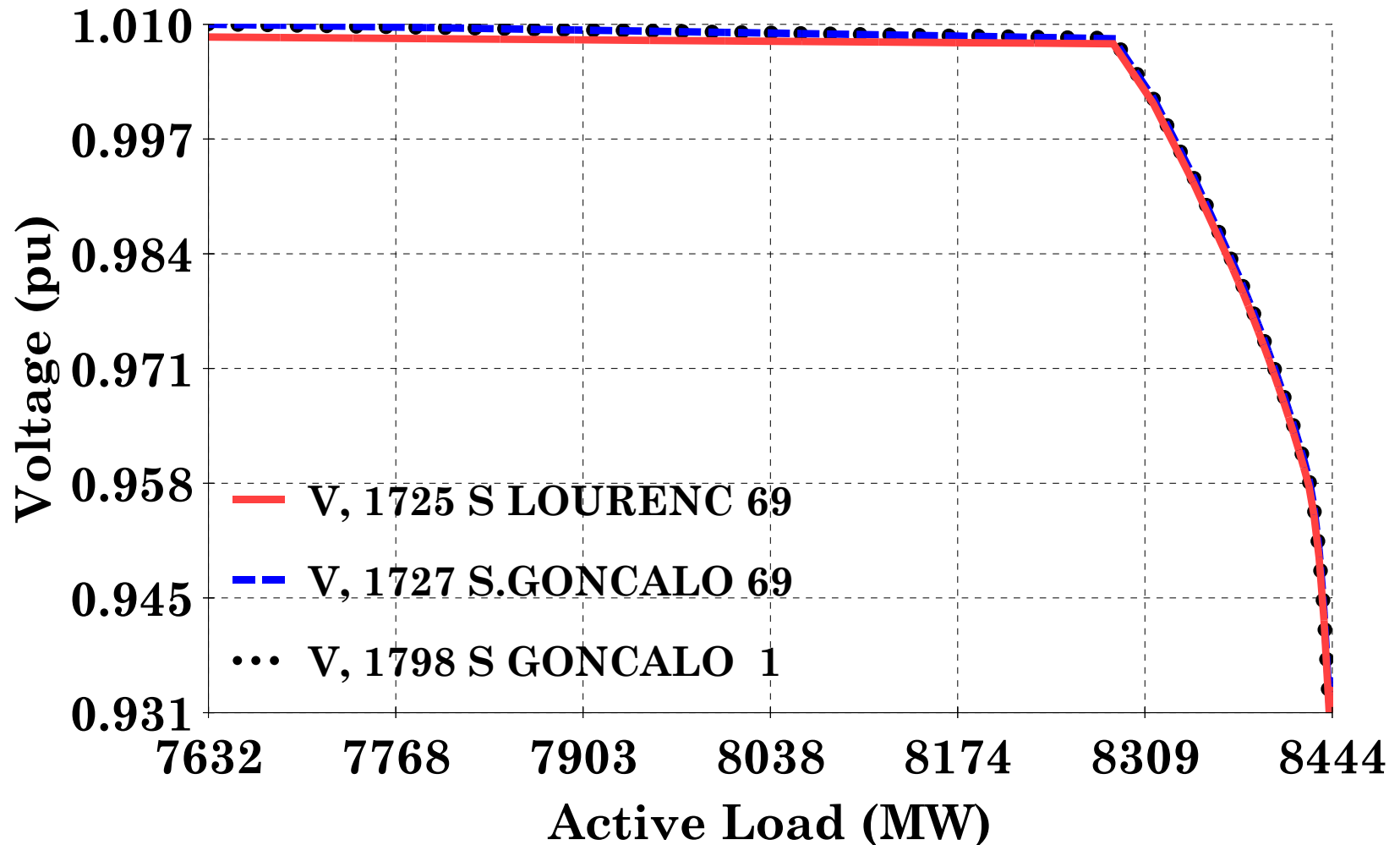
## Maximum Loadability Assessment - Rio Area

- ▶ Two cases were investigated where the Commercial induction motor load was modeled as:
  - ▶ Commercial+Feeder (Type 5)
  - ▶ Small Industrial (Type 4)
- ▶ The Industrial induction motor load was modeled as Large Industrial (Type 2)
  - ▶ This load remains fixed at the base case value



# Maximum Loadability Assessment - Rio Area

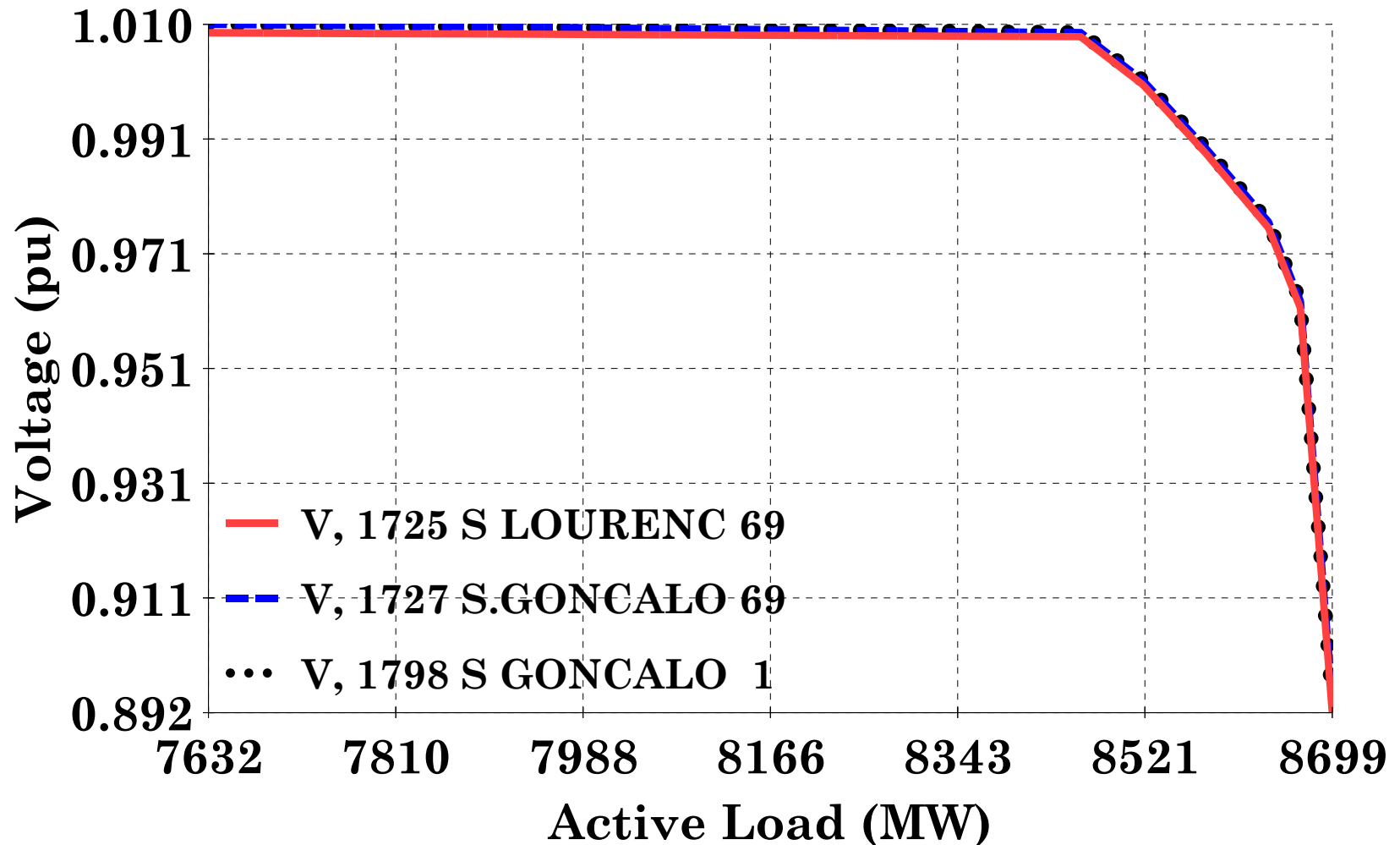
- ▶ Commercial induction motor modeled as Comm.+Feeder





# Maximum Loadability Assessment - Rio Area

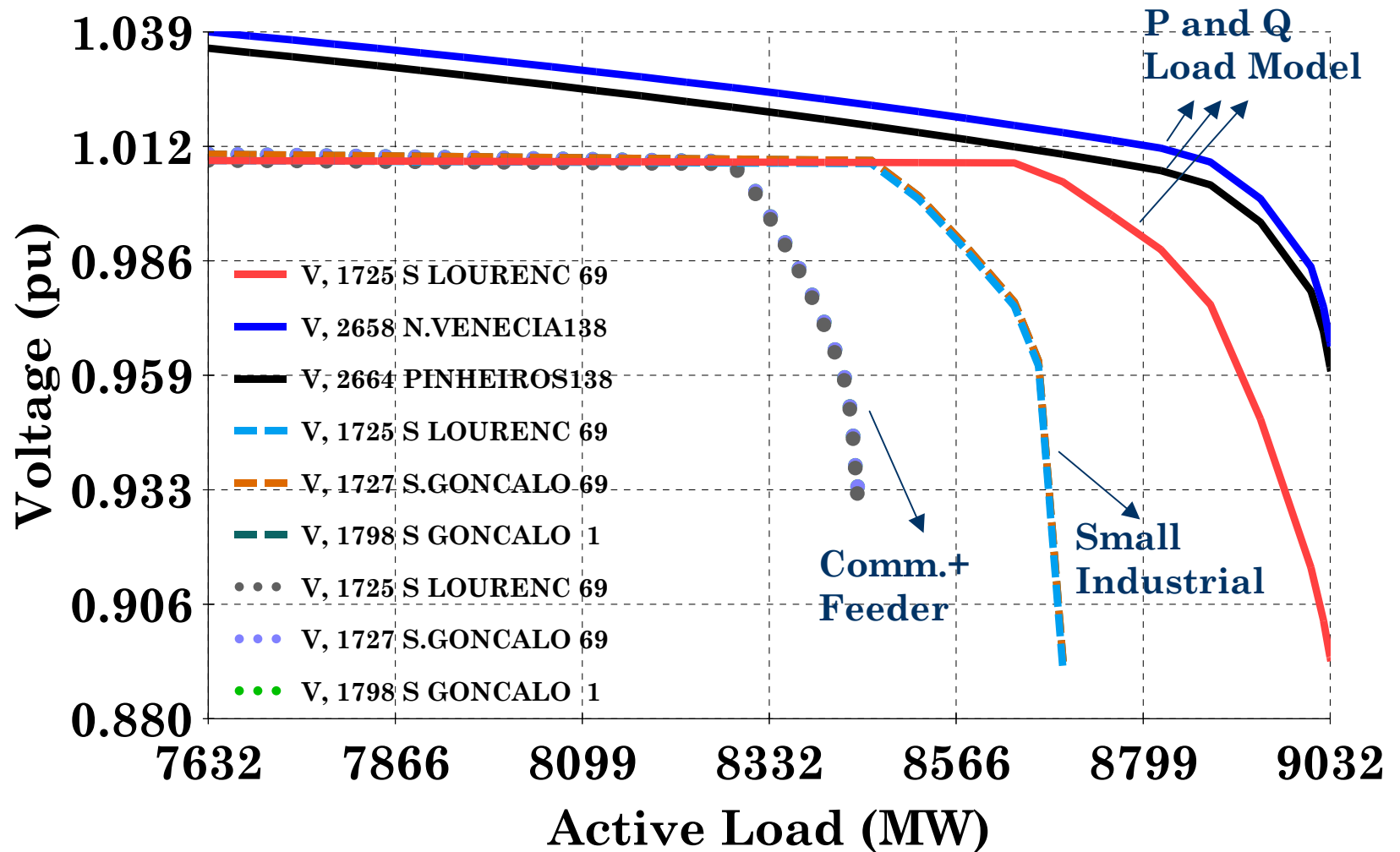
- ▶ Commercial induction motor modeled as Small Industrial





# Maximum Loadability Assessment - Rio Area

▶ Maximum loadability for 3 different load models





# Maximum Loadability Assessment - Rio Area

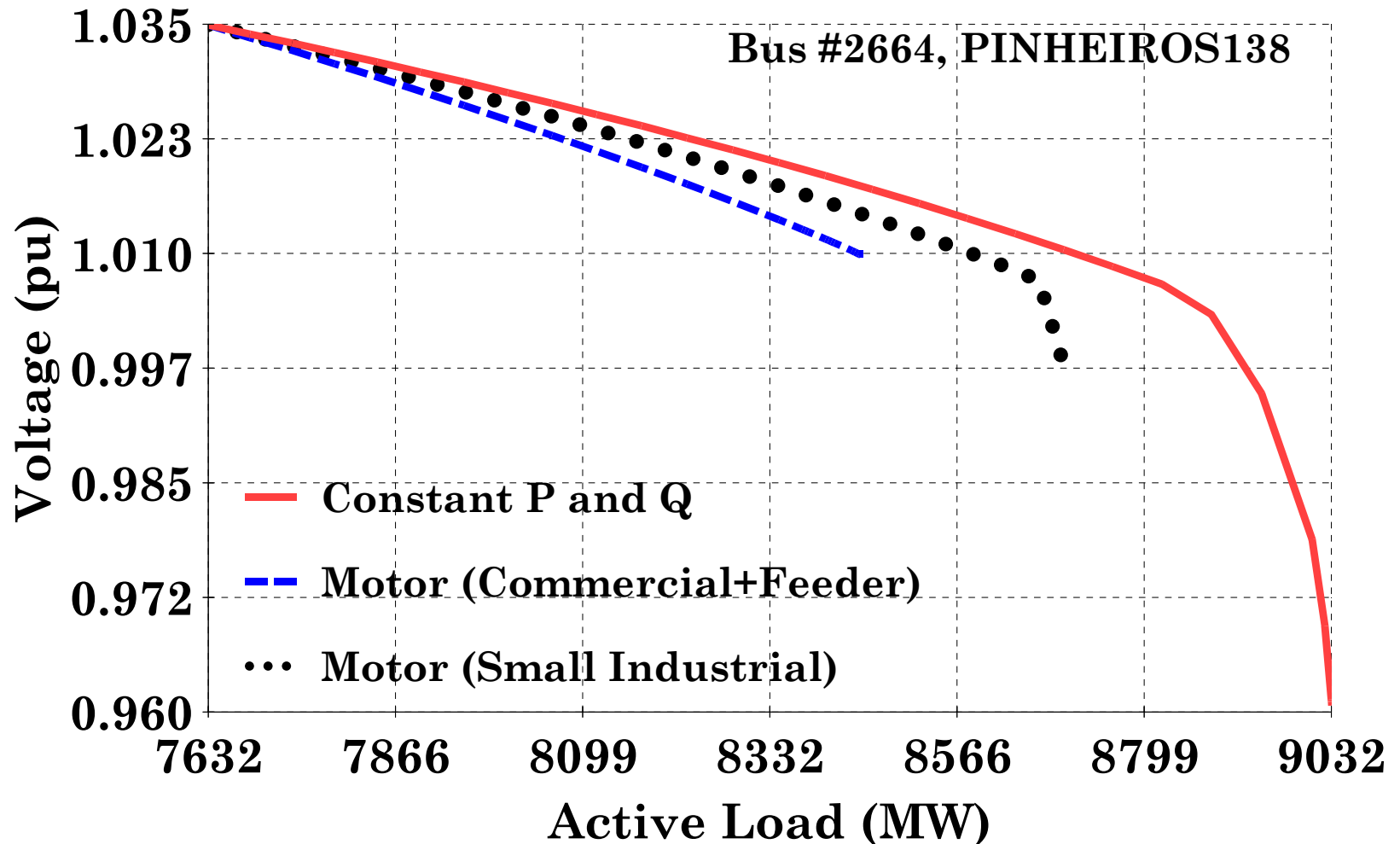
- ▶ Maximum loadability for 3 different load models

<b><i>Load Model</i></b>	<b><i>Rio Area Active Load</i></b>		
	<b><i>Initial Load (MW)</i></b>	<b><i>Induction Motor (MW)</i></b>	<b><i>Maximum Loadability (MW)</i></b>
<b>Constant P and Q</b>	<b>7632</b>	<b>-</b>	<b>9032</b>
<b>Induction Motor 4</b>	<b>7632</b>	<b>5733</b>	<b>8699</b>
<b>Induction Motor 5</b>	<b>7632</b>	<b>5733</b>	<b>8444</b>



# Maximum Loadability Assessment - Rio Area

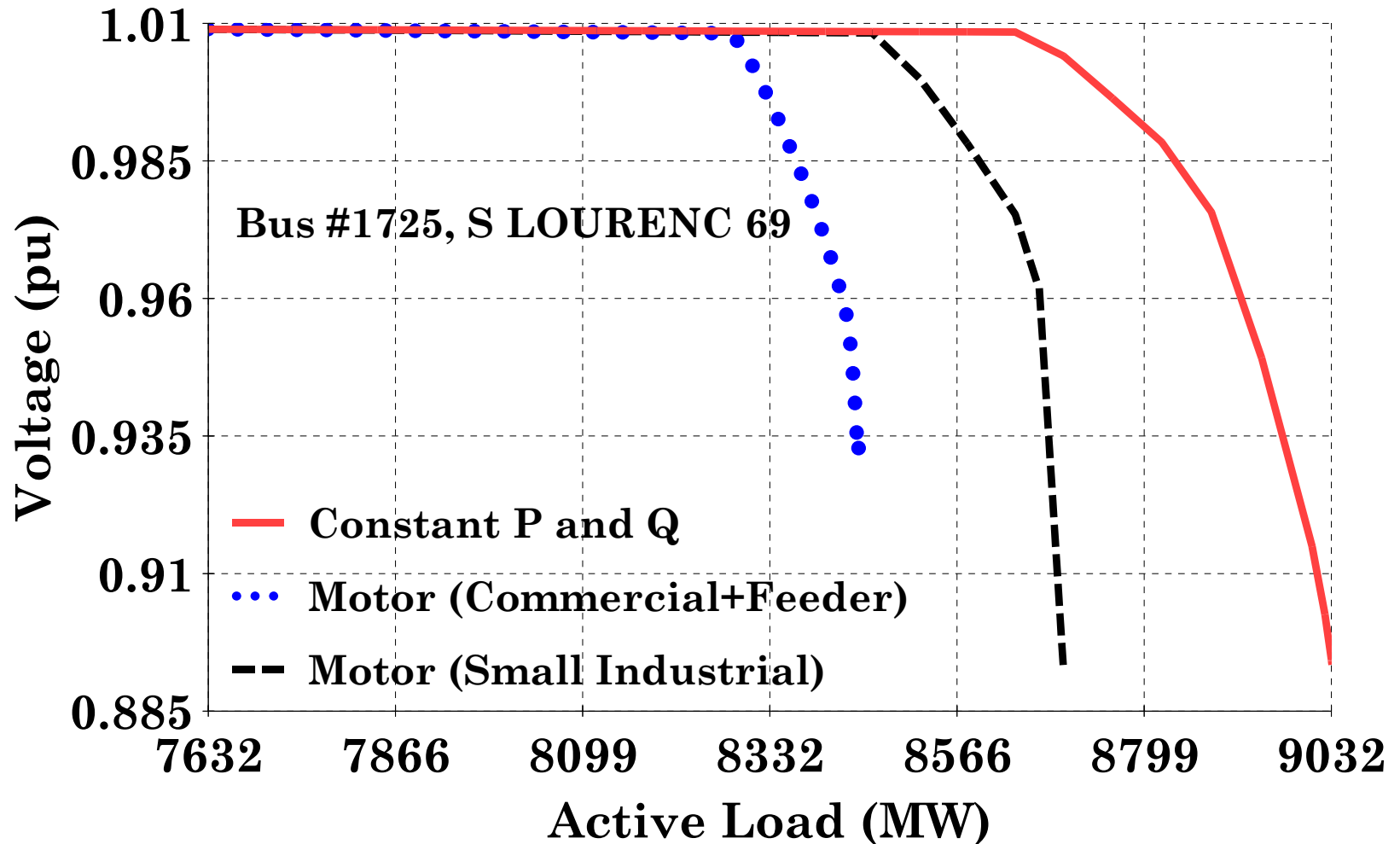
► PxV Curves of “Pinheiros-138 kV” for 3 scenarios





# Maximum Loadability Assessment - Rio Area

► PxV Curves of S. Lourenco - 69 kV for 3 scenarios





## Conclusions

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- ▶ Modeling the load as induction motors
  - ▶ Allows better analysis of system behavior
  - ▶ Ability to reveal voltage stability problems
  - ▶ Finding the cost-effective level of modeling for subtransmission and distribution networks is not an easy task
- ▶ The results are coherent to observed system behavior in Rio Area and would not be obtained if only constant-P and constant-I load models were utilized